

UNCLASSIFIED

AD NUMBER

ADB814201

LIMITATION CHANGES

TO:

Approved for public release; distribution is unlimited.

FROM:

Distribution authorized to DoD only; Administrative/Operational Use; DEC 1943. Other requests shall be referred to National Aeronautics and Space Administration, Washington, DC. Pre-dates formal DoD distribution statements. Treat as DoD only.

AUTHORITY

NASA TR Server website

THIS PAGE IS UNCLASSIFIED

UNCLASSIFIED

AD NUMBER

ADB814201

CLASSIFICATION CHANGES

TO:

unclassified

FROM:

restricted

AUTHORITY

NACA list dtd 28 Sep 1945

THIS PAGE IS UNCLASSIFIED

TECHNICAL NOTES

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

RESTRICTED

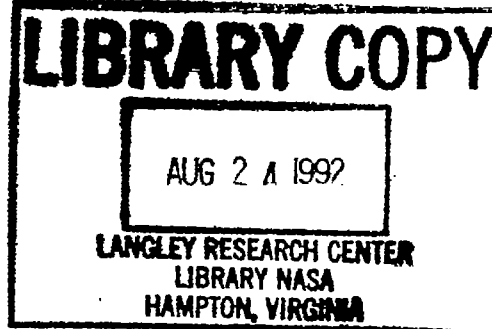
No. 920

BEARING STRENGTHS OF BARE AND ALCLAD XA75S-T
AND 24S-T81 ALUMINUM ALLOY SHEET

By R. L. Moore and C. Wescoat
Aluminum Company of America

CLASSIFIED DOCUMENT

This document contains classified information affecting the National Defense of the United States within the meaning of the Espionage Act, USC 50:31 and 32. Its transmission or the revelation of its contents in any manner to an unauthorized person is prohibited by law. Information so classified may be imparted only to persons in the military and naval Services of the United States, appropriate civilian officers and employees of the Federal Government who have a legitimate interest therein, and to United States citizens of known loyalty and discretion who of necessity must be informed thereof.



Washington
December 1943

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE NO. 920

BEARING STRENGTHS OF BARE AND ALCLAD XA75S-T
AND 24S-T81 ALUMINUM ALLOY SHEET

By R. L. Moore and C. Wescoat

INTRODUCTION

A report was recently issued covering an investigation of the bearing properties of the wrought aluminum alloys commonly used in aircraft construction (reference 1). Since this work was undertaken, two new materials, XA75S-T and 24S-T81, have been developed to the commercial stage for aircraft use. The object of this investigation was to determine the bearing yield and ultimate strengths of these new materials in the form of bare and alclad sheet.

PROCEDURE AND MATERIAL

The test procedure used in these determinations was the same as that previously described (reference 1). Figure 1 is a photograph of the test setup. Briefly, the tests involved loading single thicknesses of 0.064-inch sheet, 2 inches wide and cut parallel to the direction of rolling, in bearing on a 0.250-inch-diameter steel pin. The proportions of specimens used were the same as found to be satisfactory in previous tests. Measurements of the hole elongation were made with a filar micrometer microscope. Tests were made in triplicate for edge distances of 1.5, 2, and 4 times the pin diameter.

The material used for these tests was nominally 0.064-inch sheet. The 24S-T81 samples were commercial 24S-T sheet which had been artificially aged 12 hours at 375°F.

Tensile properties for the material are shown in table I. The values given may, with one exception, be classed as typical. The exception was the Alclad 24S-T81, for which the tensile strength was about 1 percent lower than the tentative minimum value. This difference was

not considered sufficient, however, to affect the ratios of bearing to tensile properties determined.

RESULTS AND DISCUSSION

Individual bearing test results are shown in table II. The bearing yield strength values were obtained from the bearing stress-hole elongation curves shown in figures 2 to 5, using an offset from the initial straight-line portion of the curves equal to 2 percent of the pin diameter (0.005 in.). Indicated also in table II are the types of failure obtained. Failures by the tearing out of a portion of the sheet above the pin were predominate for edge distances of 1.5 and 2 pin diameters, and by upsetting or crushing the metal above the pin for edge distances of 4 diameters.

Ratios of average bearing to tensile properties are shown in table III. The ratios for both forms of 24S-T81 are in generally good agreement with those obtained for 24S-T and the other high strength aluminum alloys in previous tests (reference 1). Although the ratios for the XA75S-T are slightly higher in most cases than for the 24S-T81, it seems advisable and not unduly conservative to place XA75S-T in the same class as 24S-T81 and the other high strength alloys, as far as ratios of bearing to tensile properties are concerned. The following ratios are proposed as typical for these newer materials.

| | Edge distance = | |
|-------------------------------|-----------------|-----------------|
| | 1.5D | 2.0D or greater |
| <u>Bearing strength</u> | 1.5 | 1.9 |
| <u>Tensile strength</u> | | |
| <u>Bearing yield strength</u> | 1.4 | 1.6 |
| <u>Tensile yield strength</u> | | |

In the report previously referred to these ratios are identical to those suggested for the other high strength aluminum alloys. Although bearing yield and

ultimate strengths do not show marked directional characteristics, it should be emphasized, as before, that the ratios given are based on tests parallel to the direction of rolling and should be applied only to tensile properties for this direction. This distinction is, of course, not necessary in the case of the 24S-T81 because this alloy does not exhibit directional characteristics in either bearing or tension.

CONCLUSIONS

The results of this investigation of the bearing properties of bare and clad XA75S-T and 24S-T81 sheet seem to warrant the following conclusions:

1. The bearing strength data obtained in this investigation are representative of materials falling within the tentative specified limits for commercial production. Table I gives a summary of tensile properties and table II gives the results of the bearing tests.

2. Average ratios of bearing to tensile strengths and bearing yield to tensile yield strengths are given in table III for tests parallel to the direction of rolling. The ratios observed for the two forms of 24S-T81 are essentially the same as previously reported for 24S-T and the other high strength aluminum alloys. The ratios for the XA75S-T are slightly higher in most cases than for the 24S-T81, although, until more data are available, it is believed that the same ratios of bearing strengths to tensile strengths should be used.

3. The following ratios of bearing to tensile properties are proposed as typical for bare and clad XA75S-T and 24S-T81 sheet. Although bearing yield and ultimate strengths do not show marked directional characteristics, it should be emphasized that when directional properties exist in tension, the ratios given apply only to the with-grain direction.

| | Edge distance = | |
|-------------------------------|-----------------|-----------------|
| | 1.5D | 2.0D or greater |
| <u>Bearing strength</u> | 1.5 | 1.9 |
| <u>Tensile strength</u> | | |
| <u>Bearing yield strength</u> | 1.4 | 1.6 |
| <u>Tensile yield strength</u> | | |

Aluminum Research Laboratories,
 Aluminum Company of America,
 New Kensington, Pa., August 11, 1943.

REFERENCES

1. Moore, R. L., and Wescoat, C.: Bearing Strengths of Some Wrought-Aluminum Alloys. T.N. No. 901, NACA, Aug. 1943.
2. Anon: Tentative Methods of Tension Testing of Metallic Materials (E8-42), 1942 Book of A.S.T.M. Standards, Part I.

TABLE I.-- TENSILE PROPERTIES OF XA75S-T AND 24S-T81

SHEET USED FOR BEARING TESTS
[Nominal thickness, 0.064 in.]

| Alloy and temper | Sample number | Ultimate strength (lb/sq in.) | Yield strength (offset = 0.2 percent) (lb/sq in.) | Elongation in 2 in. (percent) |
|-----------------------------|---------------|-------------------------------|---|-------------------------------|
| XA75S-T | 52618 | 72,500 | 63,800 | 14.0 |
| Alclad XA75S-T ⁱ | 52611 | 72,200 | 62,100 | 13.0 |
| 24S-T81 | 59381 | 72,200 | 65,100 | 6.5 |
| Alclad 24S-T81 ⁱ | 39225 | 63,500 | 57,900 | 7.0 |

Note: The above values are results of single tests in with-grain direction. Type of specimen shown in fig. 2 of reference 2.
ⁱ5 percent alclad coating on each side.

TABLE III.-- AVERAGE RATIOS OF BEARING TO TENSILE STRENGTH
FOR XA75S-T AND 24S-T81 SHEET

| Alloy and temper | Edge distance = 1.5 x pin diam. | | | Edge distance = 2 x pin diam. | | | Edge distance = 4 x pin diam. | | |
|------------------|---------------------------------|-----------|-----------|-------------------------------|-----------|-----------|-------------------------------|-----------|-----------|
| | BS TS | BYS TS | TYS TS | BS TS | BYS TS | TYS TS | BS TS | BYS TS | TYS TS |
| XA75S-T | 1.72 | 1.32 | 1.51 | 2.23 | 1.50 | 1.71 | 2.61 | 1.58 | 1.79 |
| Alclad XA75S-T | 1.62 | 1.22 | 1.42 | 2.08 | 1.38 | 1.61 | 2.35 | 1.47 | 1.71 |
| 24S-T81 | 1.45 | 1.28 | 1.42 | 1.97 | 1.43 | 1.59 | 2.39 | 1.46 | 1.62 |
| Alclad 24S-T81 | 1.54 | 1.33 | 1.46 | 2.06 | 1.46 | 1.61 | 2.48 | 1.51 | 1.65 |

Note: All bearing tests on 1/4-in. diam. steel pin (D/t = 4). Specimens 2 in. wide loaded parallel to direction of grain.

BS - bearing strength
BYS - bearing yield strength (offset = 0.02 x pin diam. = 0.005 in.)
TS - tensile strength (with grain)
TYS - tensile yield strength (offset = 0.02 percent) (with grain)

TABLE II.- BEARING STRENGTHS OF XA75S-T AND 24S-T81 SHEET

[Nominal thickness, 0.064 in.]

| Alloy and temper | Test number | Bearing strengths (lb/sq in.) | | | | | | | | |
|-----------------------------|-------------|------------------------------------|--------------------|------------------------------|----------------------------------|--------------------|------------------------------|----------------------------------|--------------------|------------------------------|
| | | Edge distance = 1.5 x pin diam. | | Type of failure ² | Edge distance = 2 x pin diam. | | Type of failure ² | Edge distance = 4 x pin diam. | | Type of failure ² |
| | | Ultimate | Yield ¹ | | Ultimate | Yield ¹ | | Ultimate | Yield ¹ | |
| XA75S-T | 1 | 125,600 | 97,000 | S | 162,500 | 109,000 | S | 178,800 | 170,000 | B |
| | 2 | 123,800 | 96,000 | S | 159,400 | 108,000 | S | 206,300 | 114,500 | B |
| | 3 | 125,000 | 96,000 | S | 163,100 | 110,000 | S | 182,500 | 118,000 | B |
| | Av. | 124,800 | 96,300 | | 161,700 | 109,000 | | 189,200 | 114,200 | |
| Alclad XA75S-T ³ | 1 | 117,500 | 89,000 | S | 148,500 | 98,000 | S | 180,400 | 105,500 | B |
| | 2 | 116,600 | 87,000 | S | 151,500 | 100,000 | S | 165,400 | 106,500 | B |
| | 3 | 116,600 | 88,000 | S | 150,300 | 101,000 | S | 164,100 | 106,500 | B |
| | Av. | 116,900 | 88,000 | | 150,100 | 99,700 | | 170,000 | 106,200 | |
| 24S-T81 | 1 | 106,000 | 94,000 | S | 143,300 | 104,000 | S | 186,900 | 107,000 | B |
| | 2 | 104,600 | 93,000 | S | 144,500 | 102,000 | S | 179,000 | 106,500 | B |
| | 3 | 102,400 | 91,000 | S | 139,400 | 104,000 | S | 152,100 | 103,500 | B |
| | Av. | 104,300 | 92,700 | | 142,400 | 103,500 | | 172,700 | 105,700 | |
| Alclad 24S-T81 ³ | 1 | 97,500 | 84,000 | S | 132,300 | 95,000 | S | 146,800 | 97,500 | B |
| | 2 | 96,800 | 84,000 | S | 132,300 | 93,000 | B | 162,700 | 96,000 | B |
| | 3 | 98,700 | 85,000 | S | 127,800 | 91,000 | B | 162,000 | 94,000 | B |
| | Av. | 97,700 | 84,500 | | 130,800 | 93,000 | | 157,200 | 95,800 | |

Note: All tests on 1/4 in. diam. steel pin ($D/t = 4$). Specimens 2 in. wide loaded parallel to direction of grain.

¹Stress corresponding to offset of 2 percent of hole diameter from initial straight-line portion of bearing stress-hole elongation curves shown in figs. 2 to 5 (0.005 in. offset for 1/4-in. diam. pin).

²Type of failure: B - Bearing, S - shear.

³5 percent alclad coating on each side.

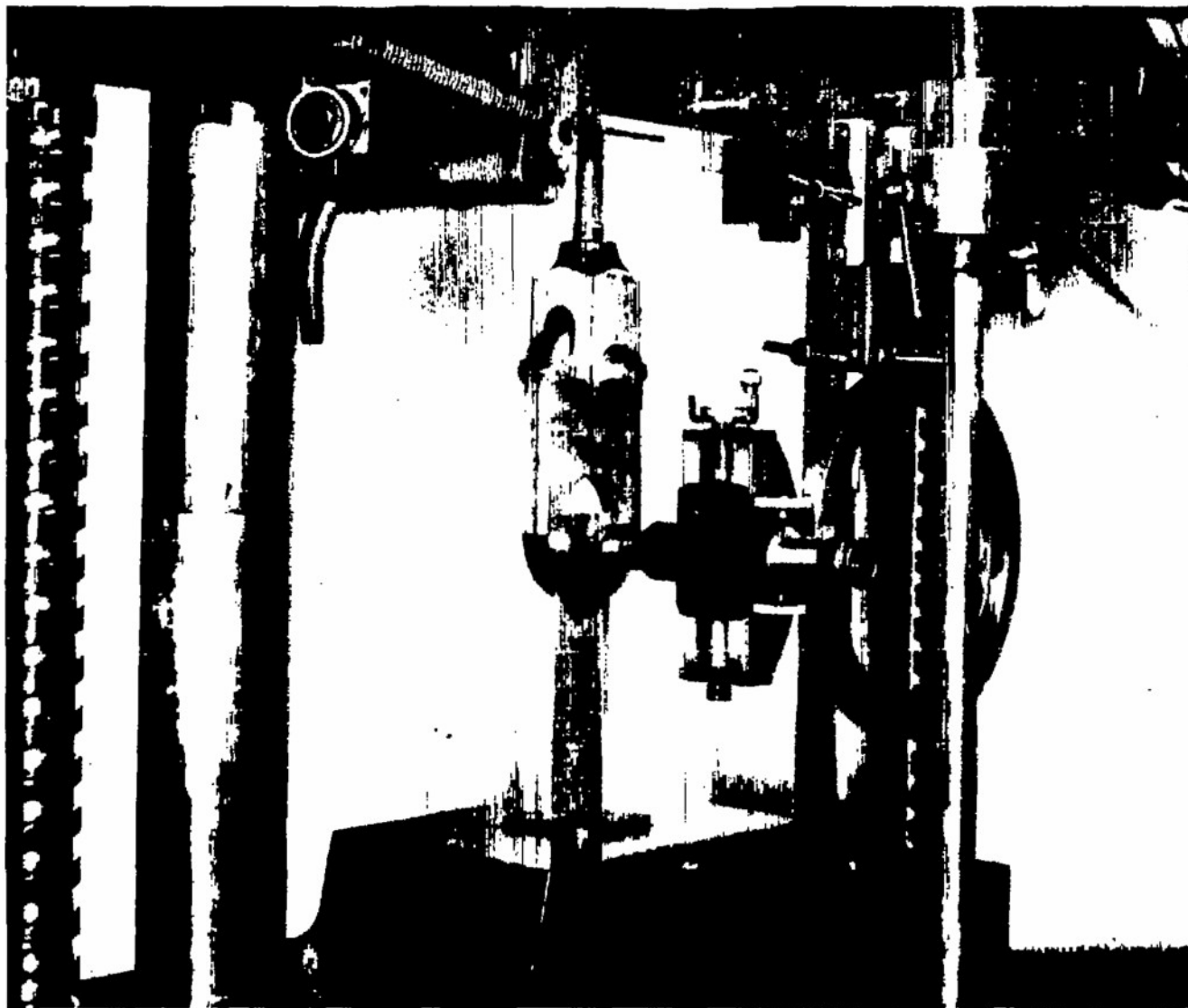
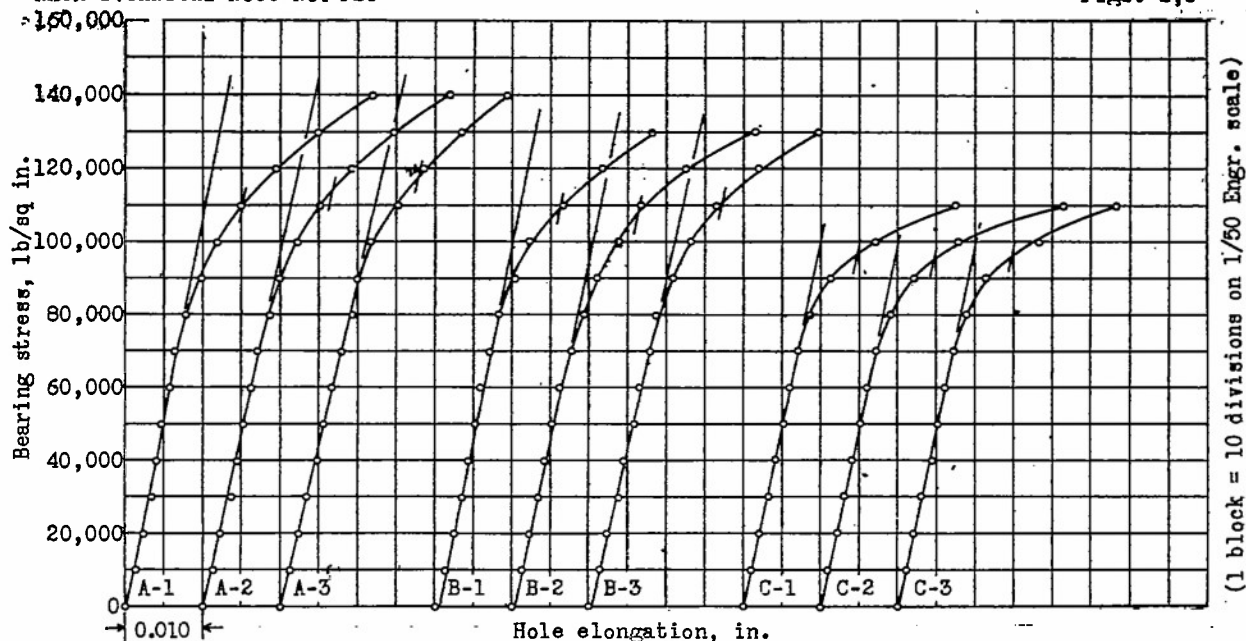


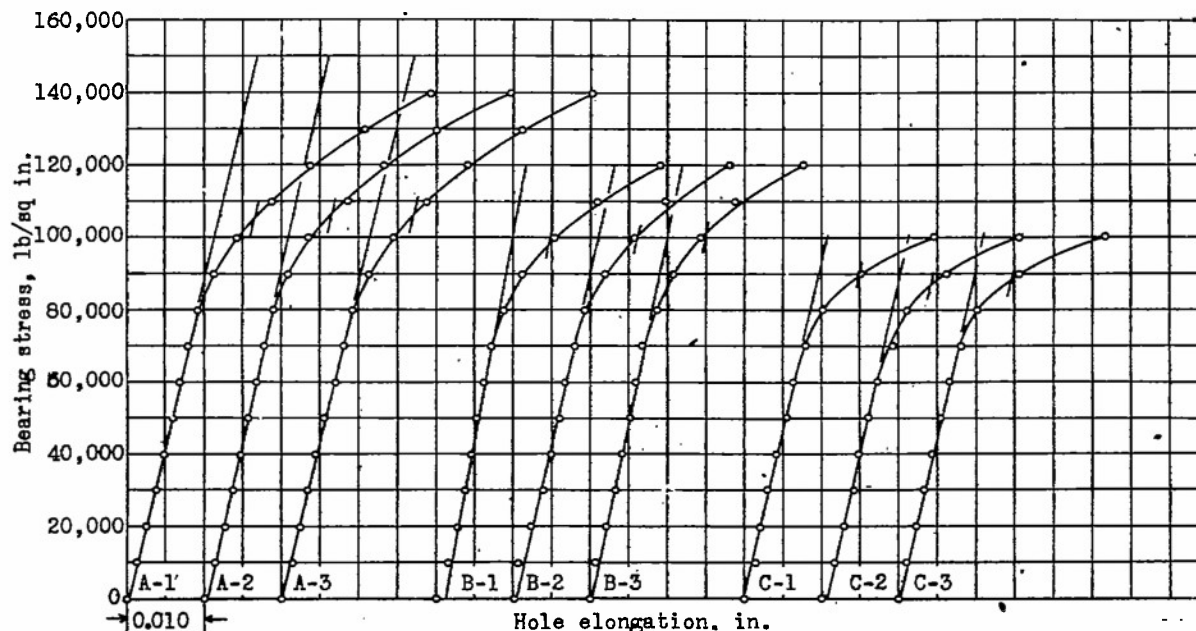
Figure 1.- Arrangement for bearing tests using Filar micrometer microscope for measurements of hole elongation.



Pin diameter = 1/4 in.
Sheet thickness = 0.064 in.
Specimen width = 2 in.

A-1, A-2 and A-3: edge distance = 4× pin diameter
B-1, B-2 and B-3: edge distance = 2× pin diameter
C-1, C-2 and C-3: edge distance = 1.5× pin diameter

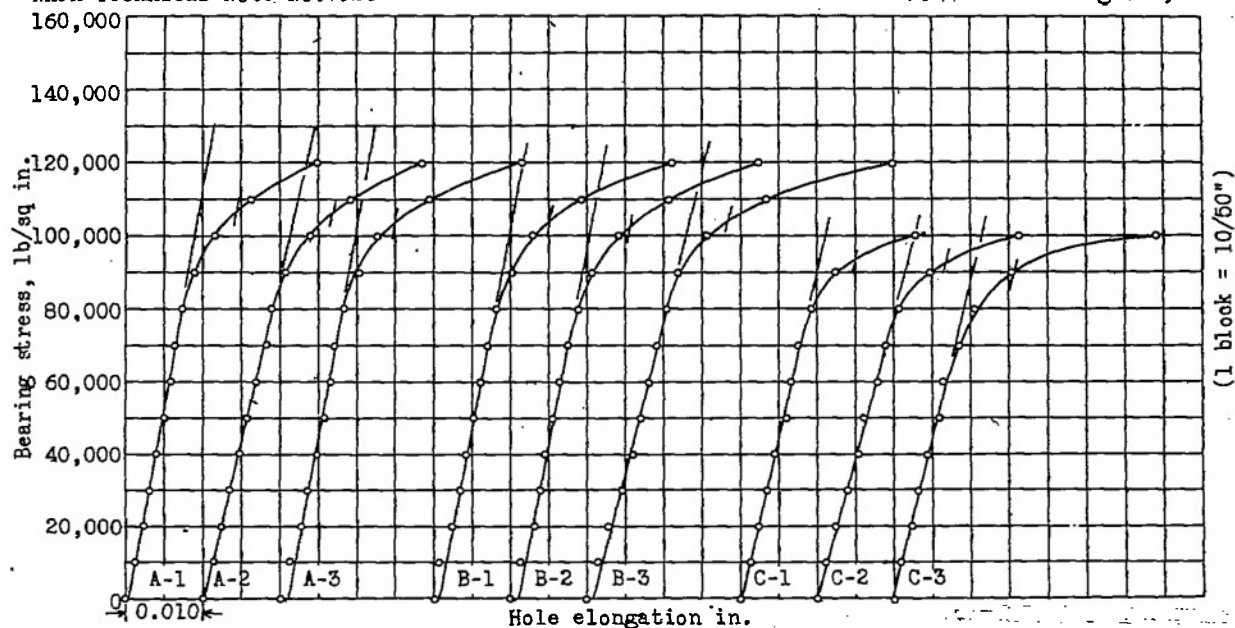
Figure 2.- Bearing stress-hole elongation curves for aluminum alloy sheet, bare
XA75S-T. Test 12-29.



Pin diameter = 1/4 in.
Sheet thickness = 0.064 in.
Specimen width = 2 in.

A-1, A-2, A-3: edge distance = 4× pin diameter
B-1, B-2, B-3: edge distance = 2× pin diameter
C-1, C-2, C-3: edge distance = 1.5× pin diameter

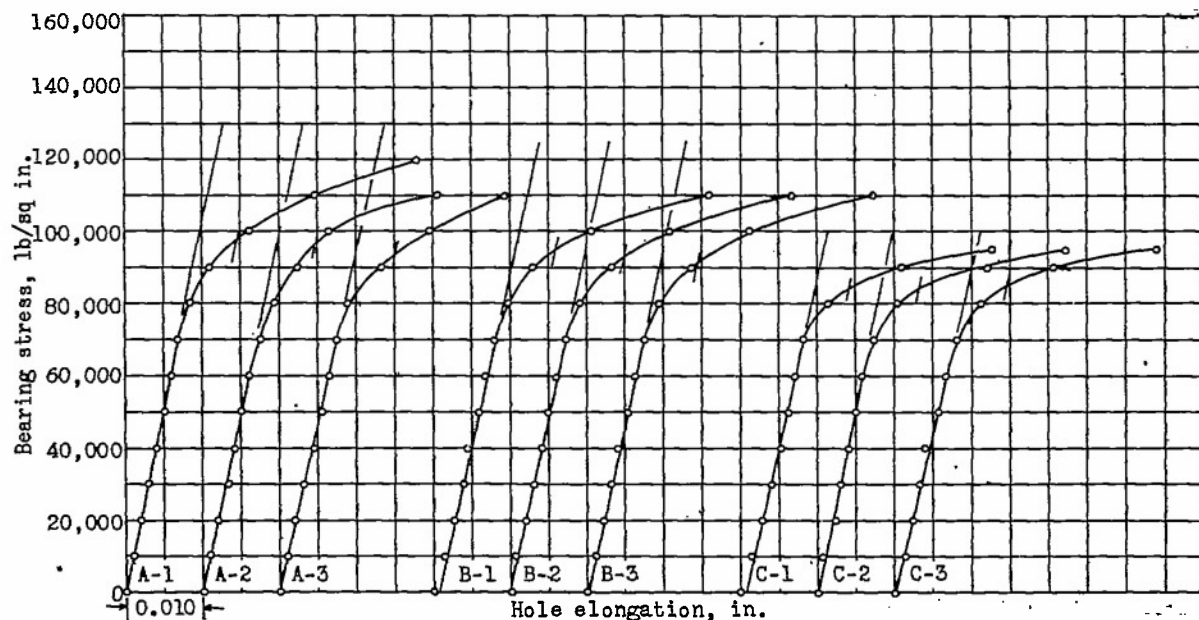
Figure 3.- Bearing stress-hole elongation curves for aluminum alloy sheet, Alclad
XA75S-T. Test 12-29.



Pin diameter = 1/4 in.
 Sheet thickness = 0.064 in.
 Specimen width = 2 in.

A-1, A-2 and A-3: edge distance = 4× pin diameter
 B-1, B-2 and B-3: edge distance = 2× pin diameter
 C-1, C-2 and C-3: edge distance = 1.5× pin diameter

Figure 4.- Bearing stress-hole elongation curves for aluminum alloy sheet, bare
 24S-T81. Test 12-29.



Pin diameter = 1/4 in.
 Sheet thickness = 0.064 in.
 Specimen width = 2 in.

A-1, A-2 and A-3: edge distance = 4× pin diameter
 B-1, B-2 and B-3: edge distance = 2× pin diameter
 C-1, C-2, and C-3: edge distance = 1.5× pin diameter

Figure 5.- Bearing stress-hole elongation curves for aluminum alloy sheet, Alclad
 24S-T81. Test 12-29.

~~RESTRICTED~~

ATI- 7-46

REVISION

TITLE: Bearing Strengths of Bare and Alclad XA75S-T and 24 S-T81 Aluminum Alloy
Sheet

AUTHOR(S): Moore, R. L. ; Wescoat, C.

ORIGINATING AGENCY: National Advisory Committee for Aeronautics, Washington, D. C.

ORIG. AGENCY NO.

TN-920

| DATE | DOC. CLASS | COUNTRY | LANGUAGE | PAGES | ILLUSTRATIONS |
|---------|------------|---------|----------|-------|------------------------|
| Dec '43 | Restr. | U.S. | Eng. | 9 | photos, tables, graphs |

ABSTRACT:

Investigation was undertaken to determine the bearing yield and ultimate strengths of XA75S-T and 24S-T81 in the form of bare and alclad sheets. The ultimate strength, yield strength, and percent of elongation of bare XA75S-T were slightly higher than those same properties of the alclad type. The ultimate strength and yield strength of bare 24S-T81 were higher than those with the alclad covering. However, the percent of elongation of alclad 24 S-T81 was higher than that of the bare type.

DISTRIBUTION: Request copies of this report only from Originating Agency

| | |
|-----------------------------------|--|
| DIVISION: Materials (6) | SUBJECT HEADINGS: Aluminum alloys - Strength (10589.6) |
| SECTION: Aluminum and Alloys (10) | |
| ATI SHEET NO.: R-8-10-9 | |

Air Material Command
U. S. Air Force

AIR TECHNICAL INDEX

Wright-Patterson Air Force Base
Dayton, Ohio

~~RESTRICTED~~

Classification cancelled
or changed to.....

AUTH:

By

Signature and Grade

Date APR 29 1949

Classification cancelled per authority
of List NACA dd. 28 Sept 1945
George R. Jordan, USCO. 29 Apr 1949